

Nickel-Technetium Separation by Metal Distillation and Vapor Deposition PACRO Presentation

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Deposition PACRO Presentation**

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Presentation By
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To
Paducah Area Community Reuse Organization
(PACRO)
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Outline

- Introduction
- Physical Properties of Nickel & Technetium
- Ni-Tc Vapor Pressures
- Phase Diagrams of Ni/Tc System
- Mass Spectrometry
- Ni/Tc Batch Distillation & Vapor Deposition
- Conclusions

Introduction

- Gas diffusion Ni barriers used in U enrichment nuclear plants (Paducah, KY) are dismantled & melted.
- 9700 tons Ni volumetrically contaminated mainly with Tc and traces of U, Pu, Th, Np and other fission products.
- Tc amount has to be lowered to undetectable limits of radioactivity for release ($\gg 1$ Bq).
- Potential Markets: Scrap metal

Introduction Cont'd

- Methods of Separating Ni from Tc used:
 - Melt refining: surface contamination
 - Conventional Electrolysis: Tc co-deposits with Ni at cathode
 - Active Carbon columns (Wako Co. Ltd.): extracts Tc but not Ni, reduces conc. to 0.5% Tc
 - Teva Resin (Eichrom): $\alpha_{Tc/Ni} = 10^4$
 - Modified Electrolysis (British Nuclear Fuel): Cleaned Ni in Oak Ridge to 1Bq but was not released
- Institute of Physical Chemistry of the Russian Academy of Science collaborating with DOE:- Tc Reduction and sorption on sludge solids, Tc uptake by noble compounds & sodium aluminosilicates.

Introduction Cont'd

- Disadvantages of above processes:
 - Do not meet required release criteria
 - Large volumes of acid has to be used => generate waste => need treatment (Purex)
- We propose the physical vapor deposition of Ni: -
 - $T_b(\text{Ni}) > T_b(\text{Tc})$
 - $P^*(\text{Ni}) \gg P^*(\text{Tc}) \Rightarrow \alpha_{\text{Tc/Ni}} > 10^6$
 - No generation of waste
 - Purification of Ni & Tc

Physical Properties

Carl Yaws, Chemical Properties Handbook, McGraw Hill, NY, 1999.

| | M_w (g/mol) | T_m (K) | T_b (K) | T_c (K) | P_c (bar) | V_c (cm ³ /mol) | ρ_c (g/cm ³) | Z_c | ω |
|----|------------------|--------------|--------------|--------------|----------------|---------------------------------|----------------------------------|-------|----------|
| Ni | 58.69 | 1728 | 2415 | 6986.15 | 4918.5 | 35.4 | 1.6566 | 0.3 | -0.17 |
| Tc | 99 | 2430 | 5000 | 17400.8 | 10183 | 42.6 | 2.2992 | 0.3 | -0.31 |

| | M_w (g/mol) | T_m (K) | T_b (K) | $\Delta H_f(T_m)$ (KJ/mol) | $\Delta H_v(T_b)$ (KJ/mol) |
|----|------------------|--------------|--------------|-------------------------------|-------------------------------|
| Ni | 58.69 | 1728 | 2415 | 17.6 | 391.85 |
| Tc | 99 | 2430 | 5000 | 23.81 | 587.93 |

Ni-Tc Vapor Pressures

Carl Yaws, Chemical Properties Handbook, McGraw Hill, NY, 1999.

$$\log(P^*) = A + B/T + C \log T + DT + ET^2 \quad P(\text{mmHg}) \quad T(\text{K})$$

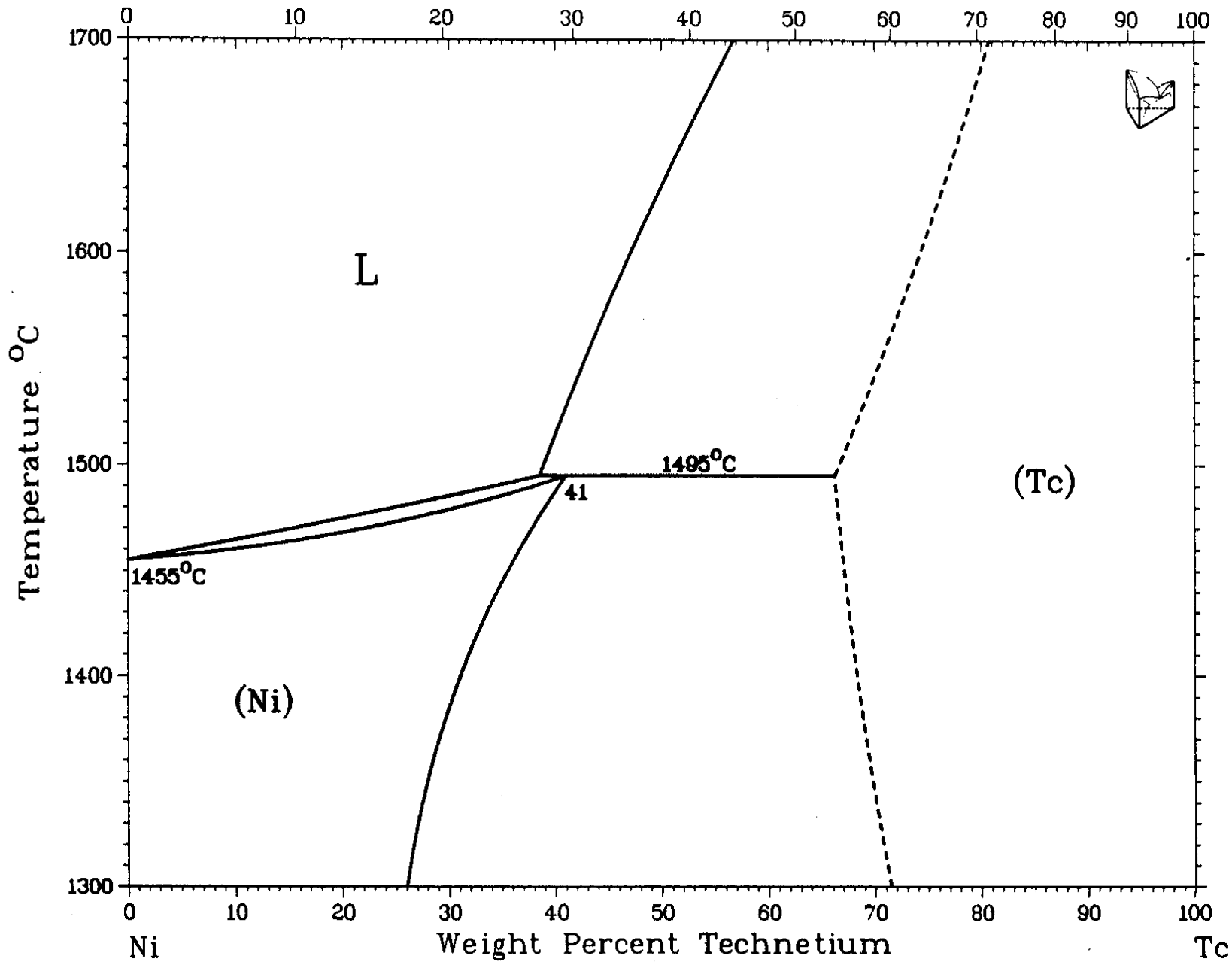
| | A | B | C | D | E | T range | T _m (K) | T _b (K) |
|----|-----------|---------|--------|-----------|----------|-----------|--------------------|--------------------|
| Ni | -57.4301 | -13533 | 23.611 | -7.67E-03 | 7.81E-07 | 1061-2415 | 1728 | 2415 |
| Tc | -240.5191 | -5792.8 | 78.794 | -1.31E-02 | 7.46E-07 | 1660-5000 | 2430 | 5000 |

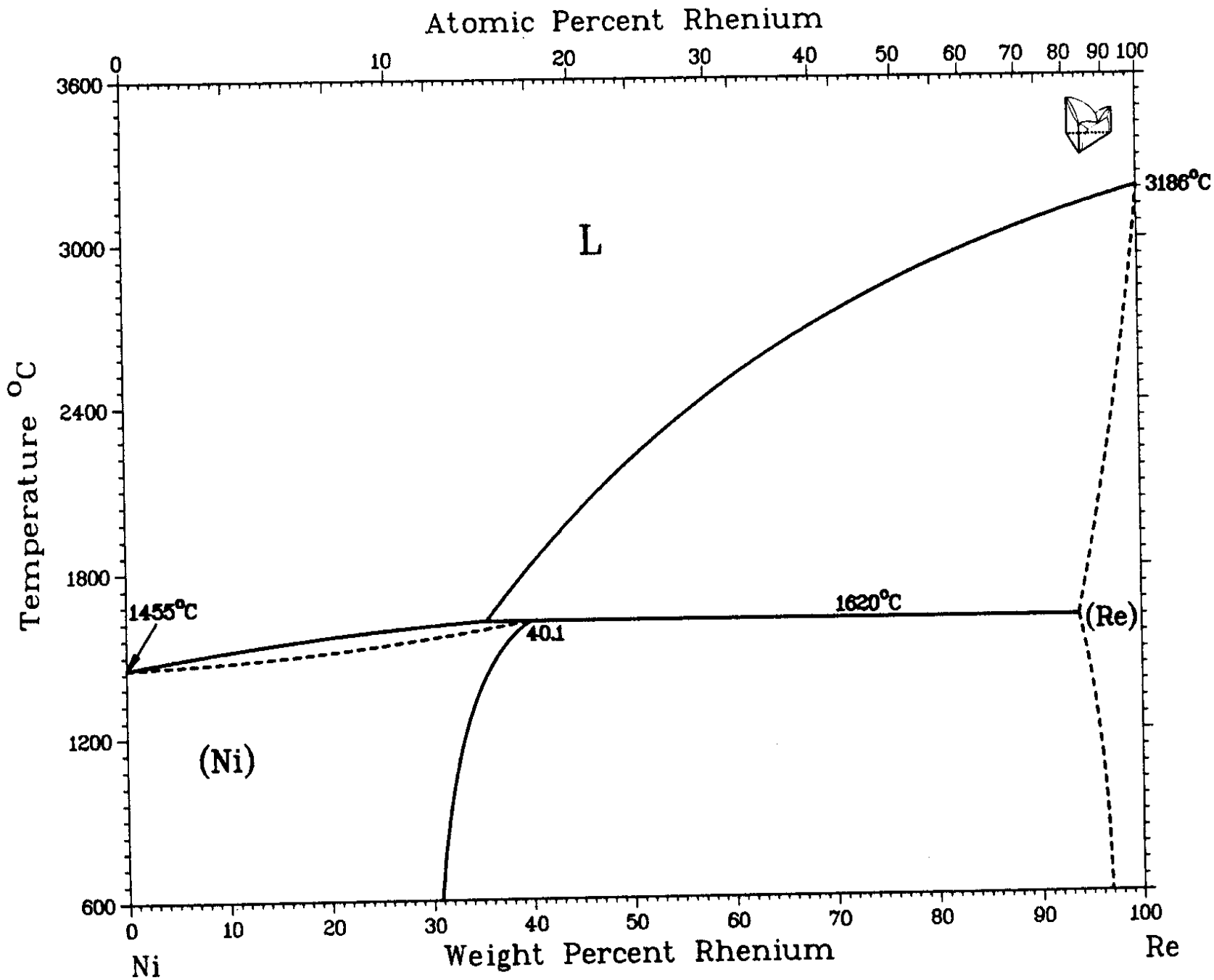
| | P* (atm) | | α |
|-------|----------|----------|----------|
| T (K) | Ni | Tc | |
| 1200 | 1.09E-07 | 5.42E-21 | 2.02E+13 |
| 1500 | 8.23E-05 | 1.01E-15 | 8.11E+10 |
| 1728 | 2.42E-03 | 8.28E-13 | 2.92E+09 |
| 2415 | 1.00E+00 | 2.77E-07 | 3.61E+06 |
| 2430 | 1.00E+00 | 3.36E-07 | 2.97E+06 |

Phase Diagrams

- Ni-Tc phase diagram (P. Nash, The Ni-Tc (Nickel-Techneium) System, *Bulletin of Alloy Phase Diagram*, Vol 6, No. 2, 1985)
- Ni-Re phase diagram (A. Nash & P. Nash, The Ni-Re (Nickel-Rhenium) System, *Bulletin of Alloy Phase Diagram*, Vol 6, No. 4, 1985)
- Area of interest: >99% wt. Ni, $T > 1455^{\circ}\text{C}$
- The phase diagrams illustrates that boiling of Ni from the mixture is possible. There are no formation of alloys.
- Initial experimentation: Ni-Re is nonradioactive & exhibits a similar phase diagram (peritectic) to Ni-Tc.

Atomic Percent Technetium





Mass Spectrometric Study

- 1) O.H. Krikorian, J.H. Carpenter, & R.S. Newbury, A Mass Spectrometric Study of the Enthalpy of Sublimation of Technetium. High Temperature Science, 1 (1969) 313-330.
- 2) Robert G. Behrens & Gary H. Rienhart, Vapor Pressure and Sublimation Enthalpy of Elemental Technetium. Journal of Less Common Metals, 75 (1980) 241-254.
- 3) Our Study

1) Krikorian et. al.

- Used a magnetic deflection mass spectrometer with a heater and an ionization source.
- Heating Element: Rhenium
- Mo is used as a standard
- Data Treatment:
 - $P = N R T$ $N = G I F$ $I = \sum_j C_{m,j}$
 - $F = (V_r m^{1/2} / \sigma B_m A t i_c) m / (\delta_{1/2})^2$
 - $A = (1 / Z) \sum_i A_i Z_j$

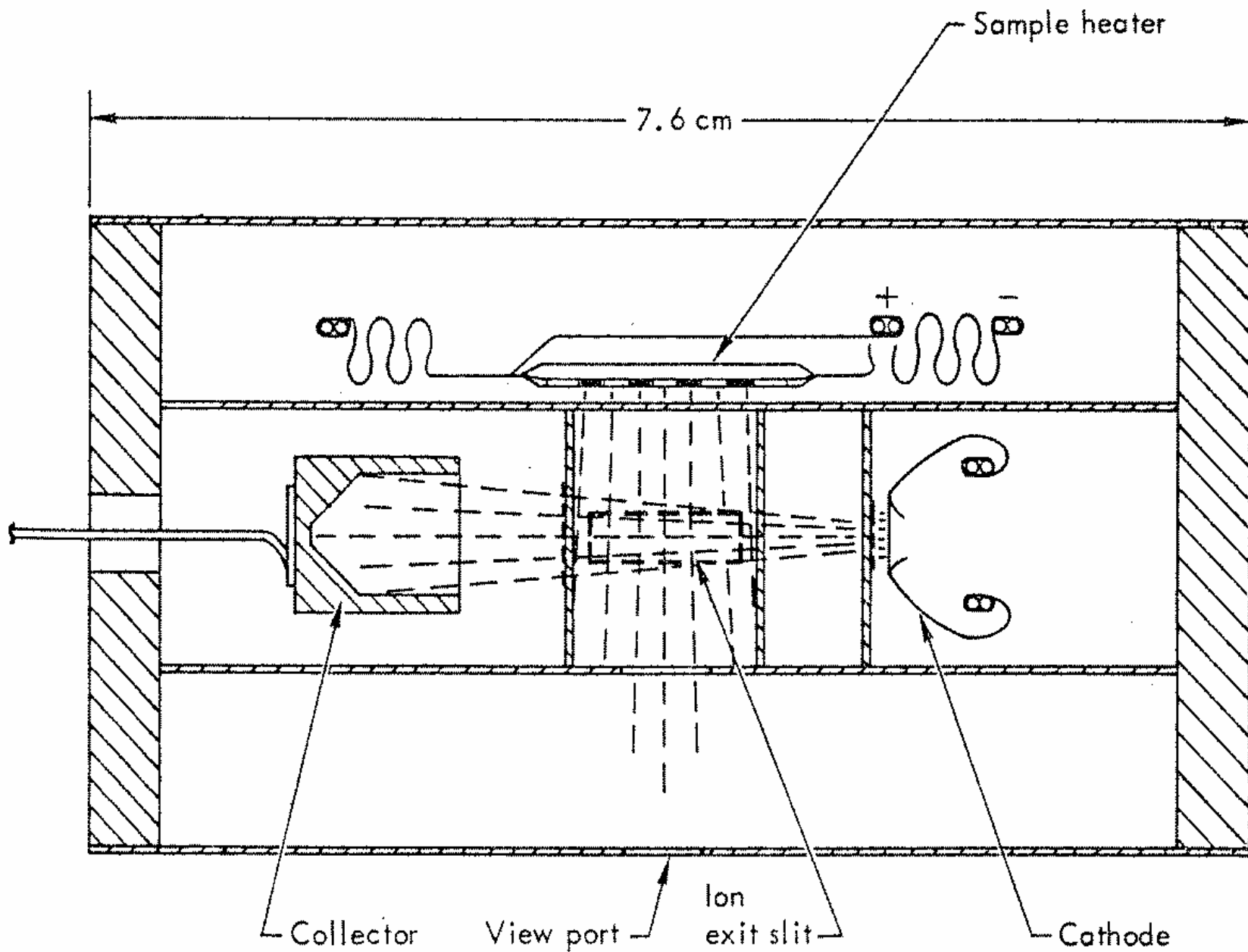


FIG. 2. Sample heater and ionization source.

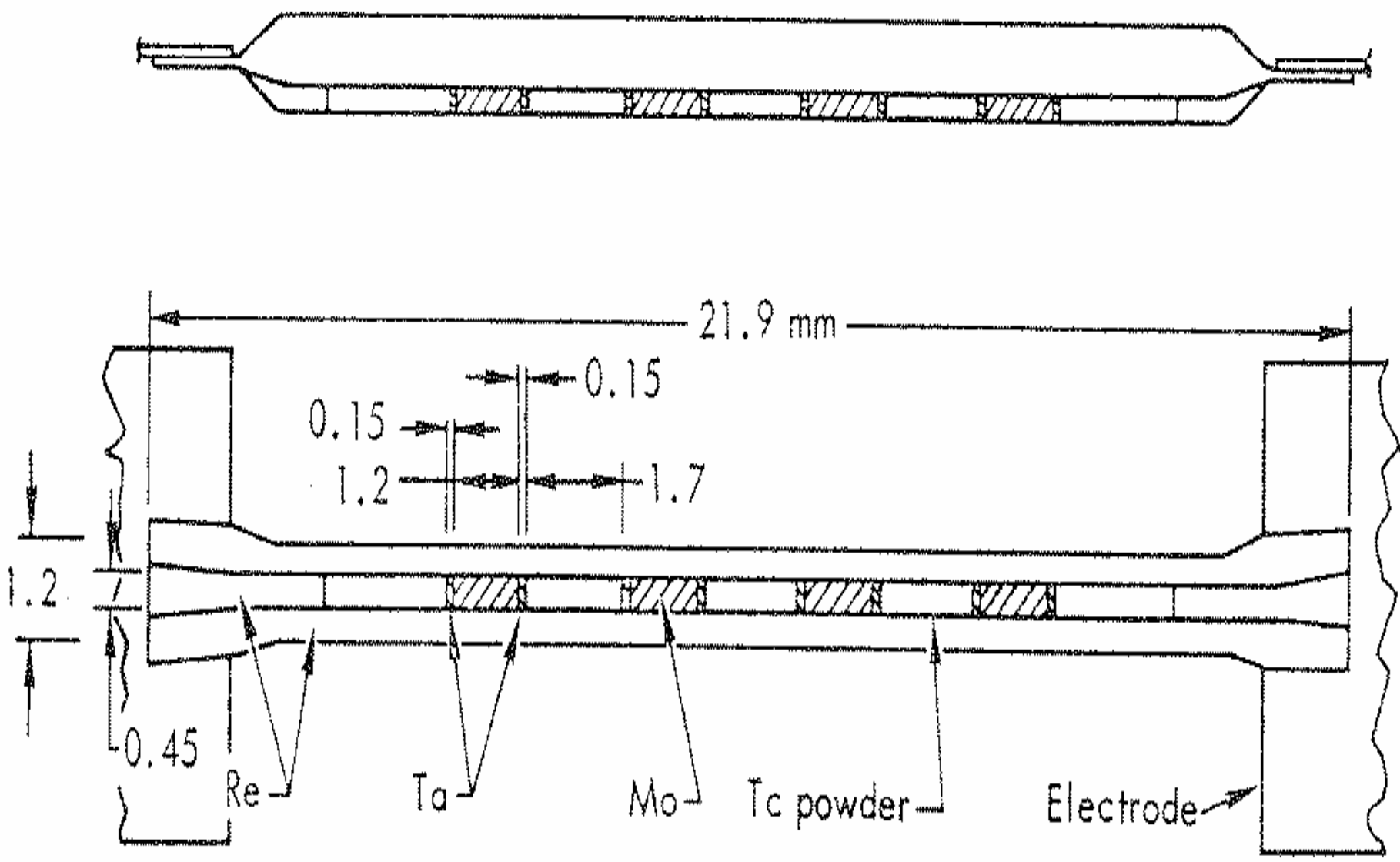


FIG. 3. Sample heater.

2) Behrens et. al.

- Used a Knudsen effusion cell mass spectrometer.
- Cell: Tantalum carbide
- Ag is used as a standard
- Data Treatment:
 - $P_{Tc} = C_s I_{Tc} T (f\sigma\gamma\tau) / (f\sigma\gamma\tau)_{Tc}$
 - $R \ln (P^*/P^0) = -\Delta H^0/T + \Delta S^0$

Comparison of Theoretical & Experimental Heats of Sublimation

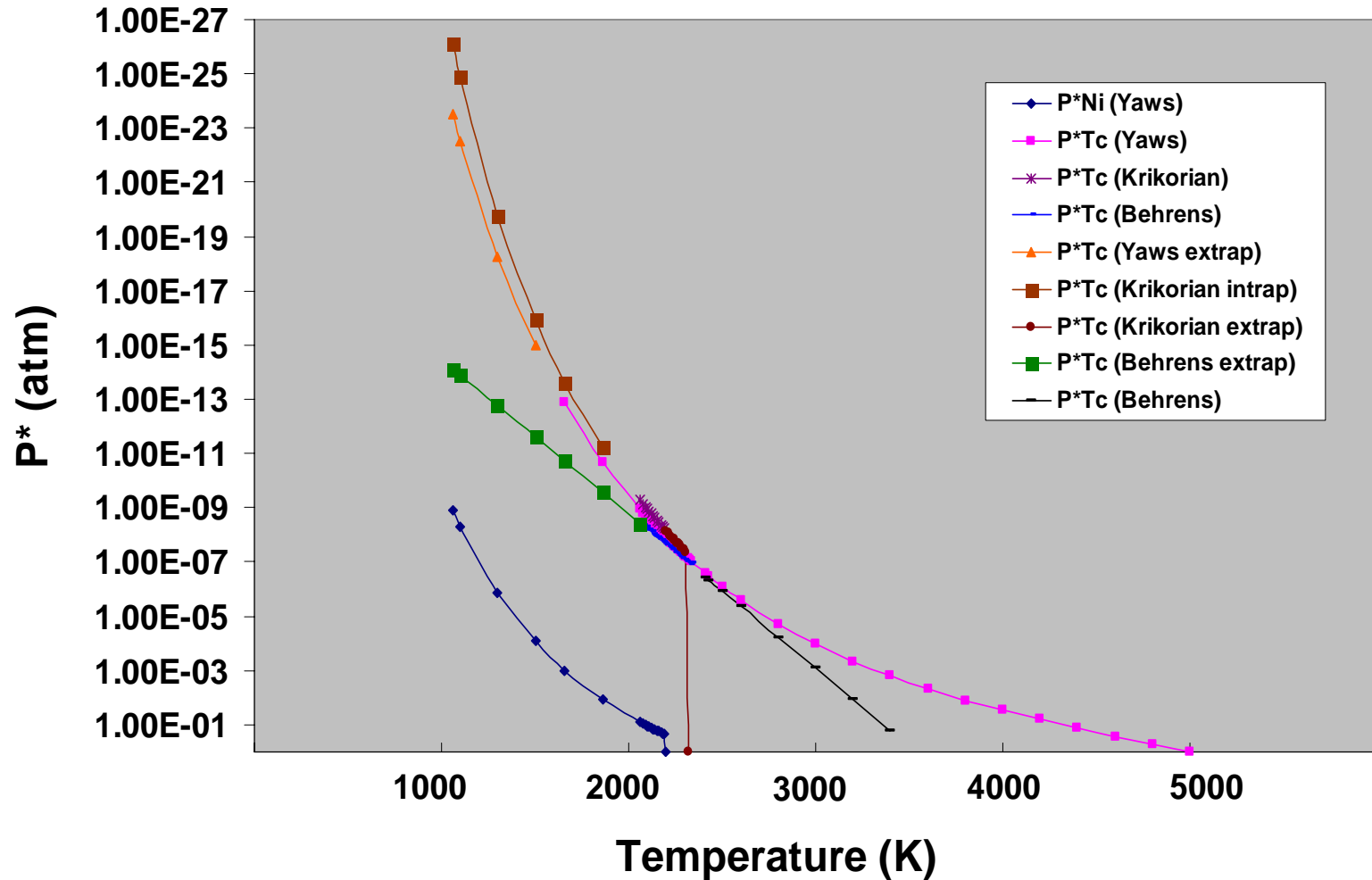
$$\Delta H_{\text{sub}} = \Delta H_{\text{fus}} + \Delta H_{\text{vap}} \text{ within 10\%error (Yaws)}$$

Exp. Error = 0.8844 % (Krokorian et. al.)

1.17096 % (Behrens et. al.)

| | | ΔH_{sub} (KJ/mol) | higher limit | lower limit |
|-------------------|----------|-------------------------------------|--------------|-------------|
| Yaws | Ni | 391.85 | 431.035 | 352.665 |
| | Tc | 587.93 | 646.723 | 529.137 |
| Krikorian et. al. | Ni (exp) | 418 | 421.69678 | 414.3032 |
| | Tc (exp) | 661.694 | 667.546 | 655.842 |
| Behrens et. al | Tc (exp) | 535.458 | 541.728 | 529.188 |

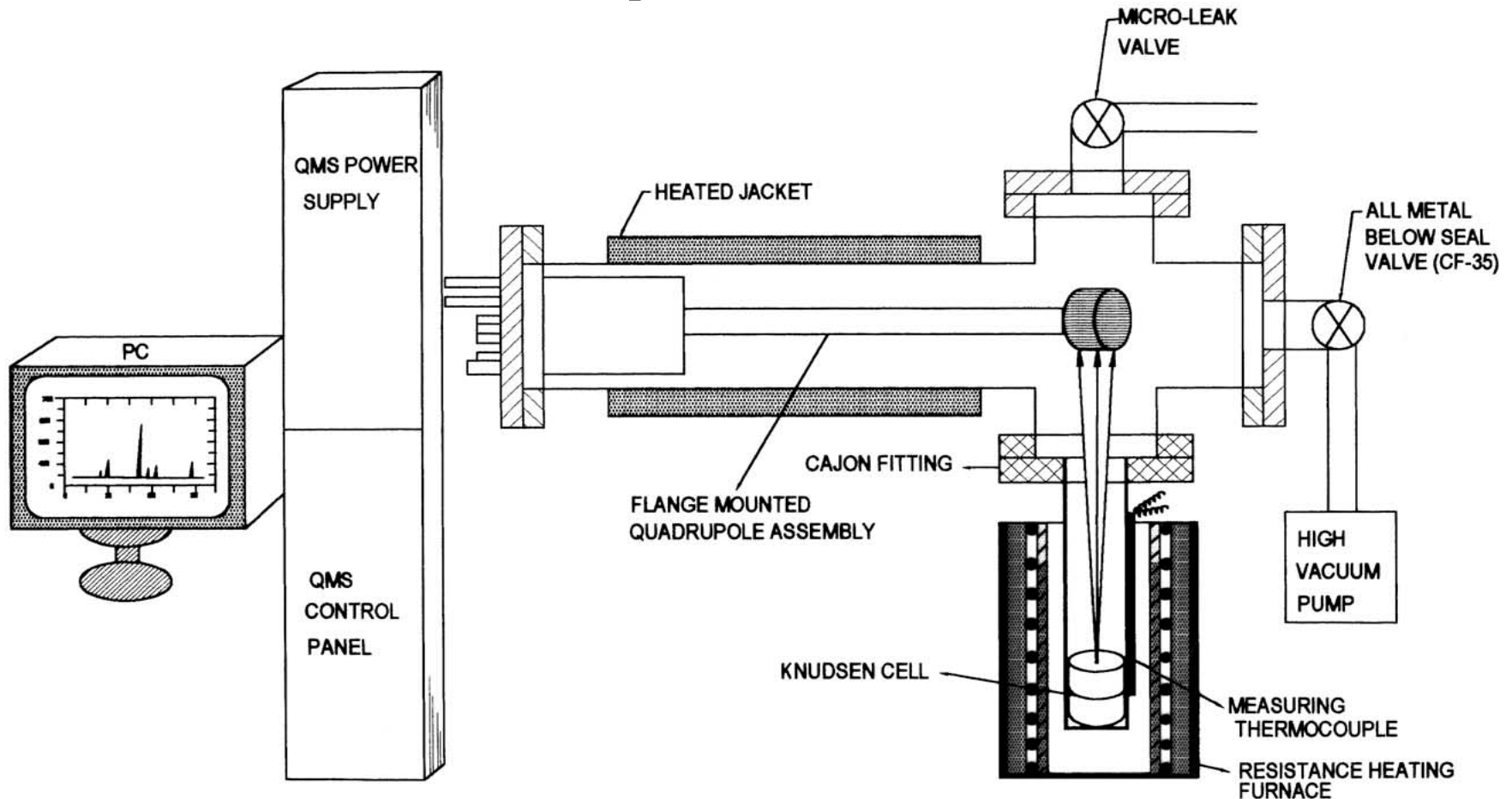
Comparison of Vapor Pressures of Tc



Our Study

- Knudsen Effusion Cell coupled to a Quadrupole Mass Spectrometer
- Cell: Tungsten
- Standard: pure Ni
- Use Data treatment:
 - $P_i = K I_i T / \sigma_i$
 - $R \ln (P^*/P^0) = -\Delta H^0/T + \Delta S^0$
 - $\ln (P^*) = \ln(I T) + \ln K + \ln \sigma_i$
 - $R \ln (I T) = -\Delta H^*/T + c$
 - $\Delta H^* - \Delta H^0 =$ enthalpy barrier for the kinetically slow steps of the vaporization process

Knudsen Effusion Cell Mass Spectrometer



Batch Distillation of Ni/Tc

- 1) 9700 tons of Ni contaminated with Tc
- 2) 10 batches for 1 year
- 3) Ni/Tc feed: 30.76g/s with 4148 ppb Tc
- 4) $T = 2430\text{K}$
- 5) $\alpha_{\text{Ni/Tc}} = 2.97 \times 10^6$
- 6) $(n_{\text{Ni}} / n_{\text{Ni}}^0 = (n_{\text{Tc}} / n_{\text{Tc}}^0)^\alpha$
- 7) $\alpha_{\text{Ni/Tc}} = P_{\text{Ni}}^* / P_{\text{Tc}}^* = (V_{\text{Ni}} / V_{\text{Tc}}) / (n_{\text{Ni}} / n_{\text{Tc}})$
- 8) Ni vapor is deposited on a cold surface & deposited to make thin sheets.

Calculation

| n_{Tc} (kmol/s) | n_{Ni} (kmol/s) | V_{Tc} (kmol/s) | V_{Ni} (kmol/s) | V'_{Tc} (kg/s) | V'_{Ni} (kg/s) | S_{Ni} (kg) | Day |
|-------------------|-------------------|-------------------|-------------------|------------------|------------------|---------------|-----|
| 4.06E-02 | 16527.45 | 4.34E-16 | 5.24E-04 | 4.E-14 | 0.0308 | 2658 | 1 |
| 4.06E-02 | 15169.03 | 4.73E-16 | 5.24E-04 | 5.E-14 | 0.0308 | 79726 | 30 |
| 4.06E-02 | 13810.61 | 5.20E-16 | 5.24E-04 | 5.E-14 | 0.0308 | 159451 | 60 |
| 4.06E-02 | 11999.38 | 5.98E-16 | 5.24E-04 | 6.E-14 | 0.0308 | 265752 | 100 |
| 4.06E-02 | 7471.31 | 9.60E-16 | 5.24E-04 | 1.E-13 | 0.0308 | 531505 | 200 |
| 4.06E-02 | 2943.24 | 2.44E-15 | 5.24E-04 | 2.E-13 | 0.0308 | 797257 | 300 |
| 4.06E-02 | 2037.63 | 3.52E-15 | 5.24E-04 | 3.E-13 | 0.0308 | 850407 | 320 |
| 4.06E-02 | 1132.02 | 6.34E-15 | 5.24E-04 | 6.E-13 | 0.0308 | 903558 | 340 |
| 4.06E-02 | 679.21 | 1.06E-14 | 5.24E-04 | 1.E-12 | 0.0308 | 930133 | 350 |
| 4.06E-02 | 452.81 | 1.58E-14 | 5.24E-04 | 2.E-12 | 0.0308 | 943421 | 355 |
| 4.06E-02 | 181.12 | 3.96E-14 | 5.24E-04 | 4.E-12 | 0.0308 | 959366 | 361 |
| 4.06E-02 | 135.84 | 5.28E-14 | 5.24E-04 | 5.E-12 | 0.0308 | 962023 | 362 |
| 4.06E-02 | 90.56 | 7.92E-14 | 5.24E-04 | 8.E-12 | 0.0308 | 964681 | 363 |
| 4.06E-02 | 45.28 | 1.58E-13 | 5.24E-04 | 2.E-11 | 0.0308 | 967338 | 364 |
| 4.06E-02 | 1.00E-07 | 7.18E-05 | 5.24E-04 | 7.E-03 | 0.0308 | 969996 | 365 |

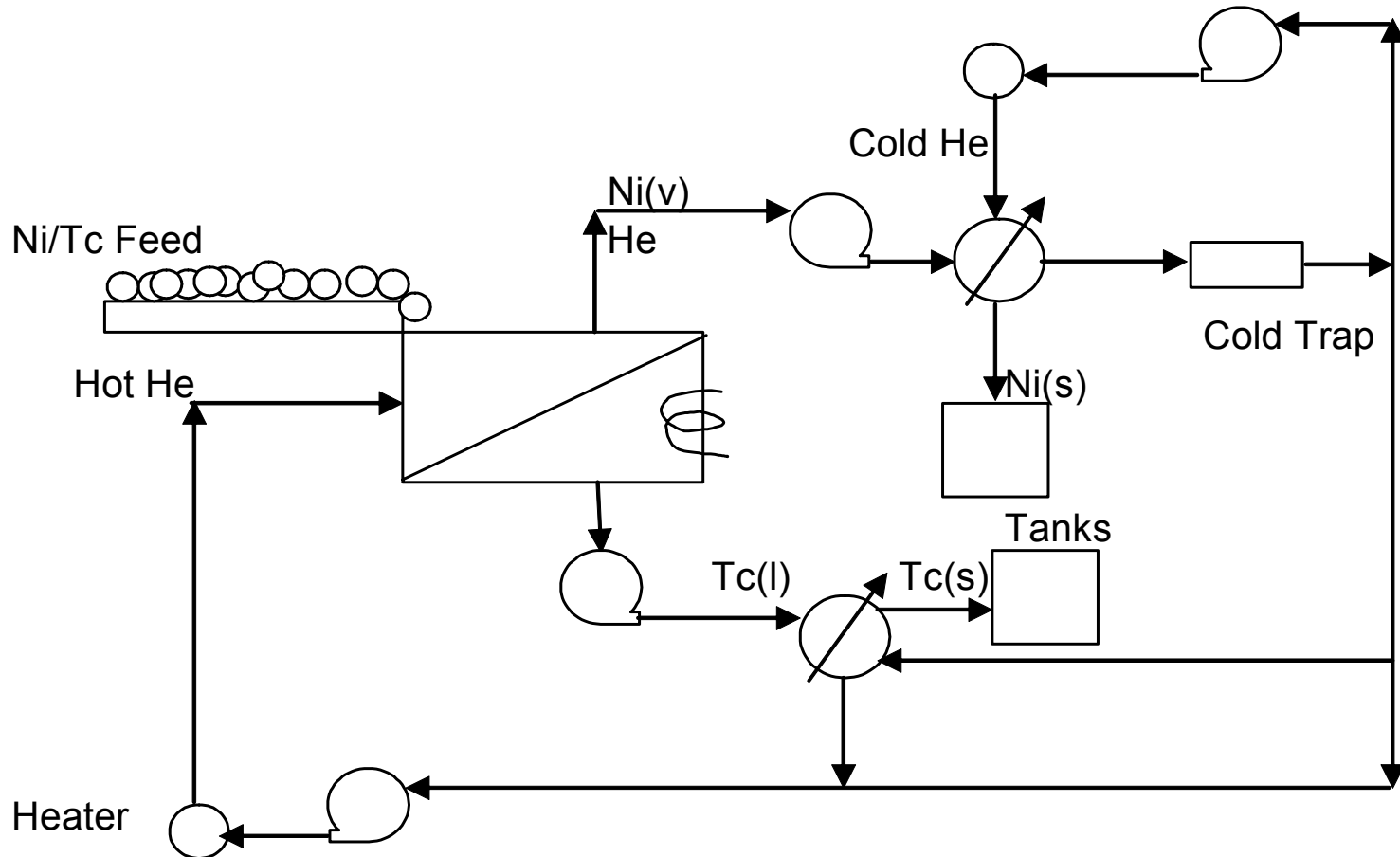
Calculation Cont'd

| x_{Tc} | x_{Ni} | y_{Tc} | y_{Ni} | y'_{Tc} | y'_{Ni} | Day |
|------------|----------|----------|----------|-----------|-----------|-----|
| 2.4591E-06 | 0.999998 | 8.28E-13 | 1 | 1.40E-12 | 1 | 1 |
| 2.68E-06 | 0.999997 | 9.03E-13 | 1 | 1.52E-12 | 1 | 30 |
| 2.94E-06 | 0.999997 | 9.91E-13 | 1 | 1.67E-12 | 1 | 60 |
| 3.39E-06 | 0.999997 | 1.14E-12 | 1 | 1.92E-12 | 1 | 100 |
| 5.44E-06 | 0.999995 | 1.83E-12 | 1 | 3.09E-12 | 1 | 200 |
| 1.38E-05 | 1.00E+00 | 4.65E-12 | 1 | 7.85E-12 | 1 | 300 |
| 1.99E-05 | 1.00E+00 | 6.72E-12 | 1 | 1.13E-11 | 1 | 320 |
| 3.59E-05 | 1.00E+00 | 1.21E-11 | 1 | 2.04E-11 | 1 | 340 |
| 5.98E-05 | 1.00E+00 | 2.02E-11 | 1 | 3.40E-11 | 1 | 350 |
| 8.98E-05 | 1.00E+00 | 3.02E-11 | 1 | 5.10E-11 | 1 | 355 |
| 2.24E-04 | 1.00E+00 | 7.56E-11 | 1 | 1.28E-10 | 1 | 361 |
| 2.99E-04 | 1.00E+00 | 1.01E-10 | 1 | 1.70E-10 | 1 | 362 |
| 4.49E-04 | 1.00E+00 | 1.51E-10 | 1 | 2.55E-10 | 1 | 363 |
| 8.97E-04 | 9.99E-01 | 3.02E-10 | 1 | 5.10E-10 | 1 | 364 |
| 1.00E+00 | 2.46E-06 | 1.20E-01 | 1 | 1.88E-01 | 1 | 365 |

Calculation Cont'd

| Tc | Activity | Recovery | Day |
|-------------|-----------------|------------------|------------|
| ppbm | Bq | of Ni (%) | |
| 1.40E-03 | 2.70E-02 | 0.27 | 1 |
| 1.52E-03 | 2.94E-02 | 8.22 | 30 |
| 1.67E-03 | 3.23E-02 | 16.44 | 60 |
| 1.92E-03 | 3.71E-02 | 27.40 | 100 |
| 3.09E-03 | 5.96E-02 | 54.79 | 200 |
| 7.85E-03 | 1.51E-01 | 82.19 | 300 |
| 1.13E-02 | 2.19E-01 | 87.67 | 320 |
| 2.04E-02 | 3.93E-01 | 93.15 | 340 |
| 3.40E-02 | 6.56E-01 | 95.89 | 350 |
| 5.10E-02 | 9.84E-01 | 97.26 | 355 |
| 1.28E-01 | 2.46E+00 | 98.90 | 361 |
| 1.70E-01 | 3.28E+00 | 99.18 | 362 |
| 2.55E-01 | 4.92E+00 | 99.45 | 363 |
| 5.10E-01 | 9.84E+00 | 99.73 | 364 |
| 1.88E+08 | 4.45E+09 | 100.00 | 365 |

Ni/Tc Separation Plant



Decontamination 9700 tons of Nickel

| | Price(\$)/kg | mass (kg) | Price (\$) for 90% Rec |
|-------------|--------------|-----------|------------------------|
| Ni Price/Kg | 6.952 | 9,699,960 | 60,690,708 |
| Tc Price/Kg | 50,000 | 40 | 1,810,602 |
| Ni / Tc | | 9700000 | 62,501,310 |

| | Cost(\$)/kg | Cost(\$)/Prod | Profit | Savings * | Savings ** |
|--------------------------|-------------|-------------------|-------------------|-------------------|-------------------|
| Electrolysis | | | | | |
| Ni (1 Bq) | 5.61 | 54,417,000 | 6,273,708 | 40,844,508 | 46,315,308 |
| Sold Ni & Tc | | | 8,084,310 | 42,655,110 | 48,125,910 |
| | | | | | |
| Nevada (disposal) | 3.564 | 34,570,800 | | | |
| | | | | | |
| Envirocare | 4.128 | 40,041,600 | | | |
| | | | | | |
| | | | | | |
| Our Process | | | | | |
| Ni (0.027-0.3 Bq) | 1.14 | 11,021,260 | 49,669,448 | 84,240,248 | 89,711,048 |
| Sold Ni & Tc | | | 51,480,050 | 86,050,850 | 91,521,650 |

* Disposal at Nevada

** Disposal at Envirocare

Conclusions

- The vaporization of Ni could be used to separate Ni from Tc due to high differences in boiling points and relative volatility.
- Mass Spectrometry is an efficient method to determine concentrations, vapor pressures, and enthalpies of Ni/Tc system.
- Batch distillation achieves higher purities of Ni & lower costs than electrorefining & electrolysis methods.

Evolution of Environmental Issues

Treatment → Sustainable Science and Engineering

End-of-Pipe Treatment

- reactive
- Reliance on abatement
- Regulation driven
- No regard for resource consumption
- Low accountability

Pollution Prevention

- Reduce
- Reuse
- Recycle

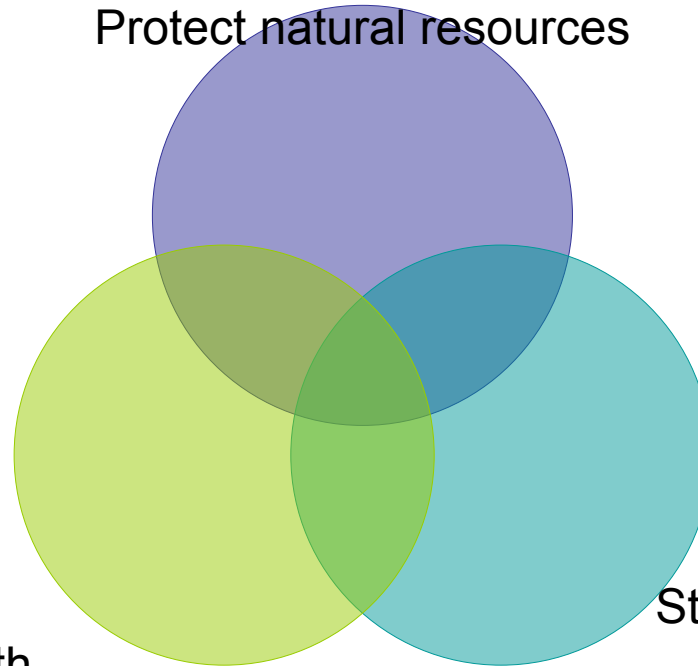
Design for environment

- Proactive
- Beyond compliance
- Life cycle analysis
- ISO 14000
- Extended product responsibility
- Benchmarking

Sustainable development

- Triple bottom line: economic, environmental, social
- Multifaceted accountability for public, private sectors

Environmental:
Human health
Ecosystem health
Biodiversity
Protect natural resources



Economic:
Productivity
Technological growth
Profit and employment

Societal:
Informed citizens
Stakeholder participation
Social justice
Equal opportunity
Wealth distribution